

5/13




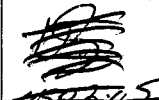
DART AEROSPACE LTD	Work Order:	22527
Description: Arm	Part Number:	D3387-041
Dwg: D3387 Rev. A	Qty:	40
		Page 1 of 1


Step	Location	Procedure	By	Date	Qty
1	DC	Issue Traveler	JS	05.02.23	40
2	MV	Cut blank: 6.000" x 0.500" x 17.800" long Material: 6061-T6/T651 (QQ-A-200/8) (M6061T6B0.500x06.000) Identify for D3387-1	M/6991 M/6953 Batch: M/6764	05.02.23	40
3	MV	Machine as per Folio FA511 and Dwg D3387 Identify as D3387-1	EC/SL	07-3-05	40
4	MV	C'sink Ø0.375" as per Dwg D3387	EC	05.03.05	40
5	QC2	Inspect parts as they come off the CNC machine	EC/SL	07-3-05	40
6	QC8	Second check	ML	05/03/07	40
7	MV	Tumble and Deburr NO sharp edges	EC/SL	05-03-07	40
8	QC5	Inspect work to Step 7	ML	05/03/07	40
9	FP	Chemical Conversion Coat as per QSI 005 4.1			
10	QC3	Inspect Chemical Conversion Coat			
11	GA	Press spacer into D3387-1 arm as per Dwg D3387 Pick: Qty Part Number Description Batch 1 D2808 Spacer			
12	QC6	Inspect work to Step 11			
13	ST	Identify and Stock	AD	05.03.08	40
14	AC	Cost / part: <u>29.75</u>	SAC	05.03.09	40
15	DC	Close W/O <u>29.75</u> Inspect Level 21	AD	05/09/19	40

Rev	Date	Change	Revised By	Approved
A	05.02.22	New Issue	KJ/JLM	

RELEASED
11/05/23

W/O:		WORK ORDER CHANGES					
DATE	STEP	PROCEDURE CHANGE	By	Date	Qty	Approval Mfg / Design Mgr	Approval QC Inspector

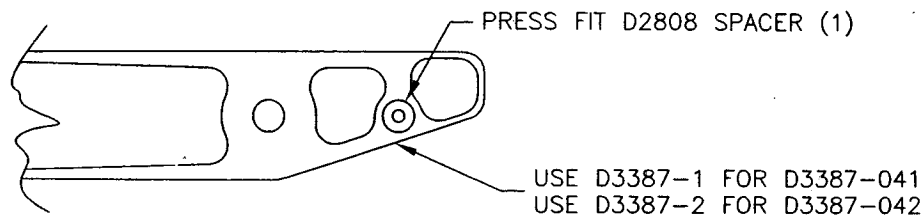
NCR:		WORK ORDER NON-CONFORMANCE (NCR)						
DATE	STEP	Description of NC Section A	Corrective Action Section B			Verification Section C	Approval Design Mgr	Approval QC Inspector
			Initial Design Mgr	Action Description Design Mgr	Sign & Date			
05-07-03	3	- 1 part is under tol, by 0.005" on 2.000 dim. should be 2.000 ^{+0.01} _{-0.005} reading 1.990"	 CP	PART IS ACCEPTABLE. MARGIN IS STILL POSITIVE.			 05.08.12	

Part No: _____ PAR #: _____ Fault Category: _____ NCR: Yes ☒ No ☐ DQA:  Date: 05/09/19

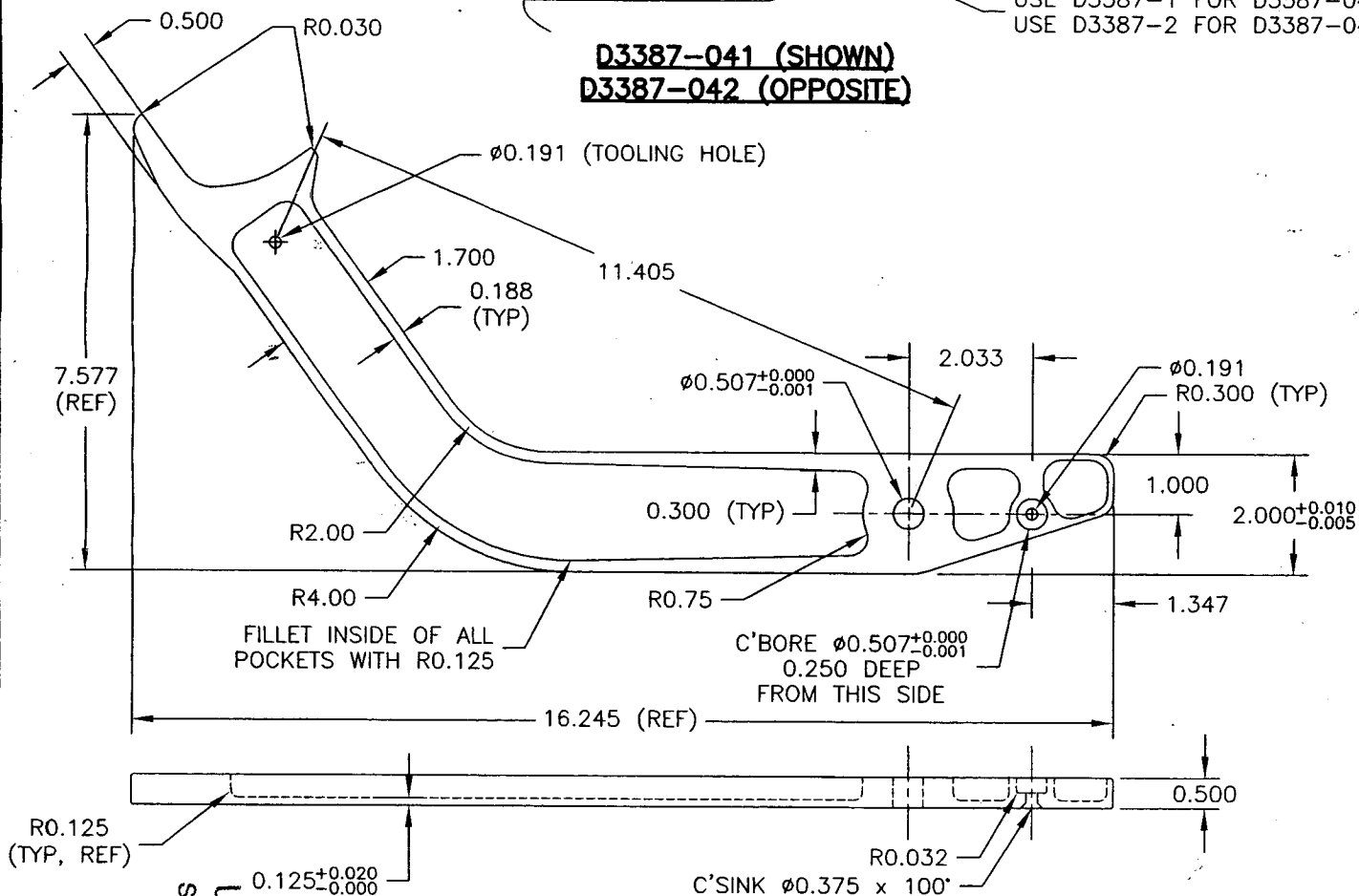
NOTE: Date & initial all entries QA: N/C Closed: _____ Date: _____

PRELIMINARY ISSUE

DESIGN	00	DRAWN BY	00	DART AEROSPACE LTD HAWKESBURY, ONTARIO, CANADA
CHECKED		APPROVED		DRAWING NO. D3387
DATE	05.01.18	TITLE	ARM	REV. A SHEET 1 OF 1
A	05.01.18	NEW ISSUE		SCALE 1:3



D3387-041 (SHOWN)
D3387-042 (OPPOSITE)



D3387-1 (SHOWN)
D3387-2 (OPPOSITE)

GENERAL NOTES

1. MACHINE PER DRAWING FILE "D3387-A.DWG"
2. MATERIAL 6061-T6 (QQ-A-200/8 OR QQ-A-250/11) 0.500 THICK (REF DART SPEC. M6061T6B0.500)
3. DEBURR TO LEAVE R0.030 - 0.063 ON ALL EDGES
4. TOLERANCES ARE PER DART QSI 018 UNLESS OTHERWISE NOTED
5. ALL DIMENSIONS ARE IN INCHES

SUBJECT TO CHANGE WITHOUT NOTICE

WORK ORDER

NO. 22527

Job Costing Report

Dart Aerospace Ltd.
Hawkesbury

Feb 22, 2005
03:39 pm

Work Order No : 0022527
Project Name : D3387-041
Project For : WK513
Work Order Type : Main
Main WO Number :
House Part Number : D3387-041
Description : Arm Assembly
Manufactured : No
Amount Req'd : *0*
Amount Done : 0
Start Date : 02-22-05
Est Finish Date : 03-15-05
Act Finish Date :
Drawings Req'd : No
Ok for Approval :
Approval Rec'd :

Department Code:
Burden Flags : NNNNNNNN
WO Status : Open
Invoice State : Not Invoiced
Invoice Date :
Invoice Number :
Invoice Amount : 0.00
Order Entry No :
OE Value : 0.00
Est Margin : 0.000%
Actual Margin : 0.000%
\$0 Posted to Finished Goods

	Estimated	Actual	Var. %	Posted	To Post
Material Cost :	0.00	0.00	0.00	0.00	0.00
Engineering Hours :	0.00	0.00	0.00		
Engineering Cost :	0.00	0.00	0.00	0.00	0.00
Production Hours :	0.00	0.00	0.00		
Production Cost :	0.00	0.00	0.00	0.00	0.00
Packaging Hours :	0.00	0.00	0.00		
Packaging Cost :	0.00	0.00	0.00	0.00	0.00
OverHead Hours :	0.00	0.00	0.00		
OverHead Cost :	0.00	0.00	0.00	0.00	0.00
CNC Hours :	0.00	0.00	0.00		
CNC :	0.00	0.00	0.00	0.00	0.00
Misc. Hours :	0.00	0.00	0.00		
Misc. :	0.00	0.00	0.00	0.00	0.00
Burden :	0.00	0.00	0.00		
Total Cost :	0.00	0.00	0.00		
Margin :	0.000	0.000			
Selling Cost :	0.00	0.00			

	Estimated	Actual
Labour Hrs/Amount Done :	0.00	0.00
Profits/(Loss) :	0.00	0.00

6.2 D3387-1/-2 ARM

The D3387-1/-2 arms are used in the D412-630-023/-024 steps. The maximum load in this part corresponds to R84L = R155L determined in section 4.1 of this report. Refer to Figure 6 in Appendix D for the geometry involved in this analysis. For each critical section shown in Figure 6, the D3387-1/-2 arms are checked for bending failure.

Geometry

$$\begin{aligned} x1 &:= 12.19 \cdot \text{in} & x_a &:= 11.64 \cdot \text{in} & \theta_a &:= 35.77 \cdot \text{deg} \\ x2 &:= 1.99 \cdot \text{in} & x_b &:= 0.95 \cdot \text{in} \\ & & x_c &:= 0.60 \cdot \text{in} \\ & & x_d &:= 6.21 \cdot \text{in} \end{aligned}$$

Loads

$$\begin{aligned} F &:= R84L & F &= 765 \cdot \text{mass} & \text{Applied load} \\ M_{\text{max}} &:= F \cdot x1 & M_{\text{max}} &= 9325 \cdot \text{lb} \cdot \text{in} & \text{Maximum bending moment} \\ F_s &:= \frac{M_{\text{max}}}{x2} & F_s &= 4686 \cdot \text{mass} & \text{Load applied to the stop} \\ F_{py} &:= F + F_s \cdot \sin(\theta_a) & F_{py} &= 3504 \cdot \text{mass} & \text{Vertical load at the pivot} \\ F_{px} &:= F_s \cdot \cos(\theta_a) & F_{px} &= 3802 \cdot \text{mass} & \text{Horizontal load at the pivot} \\ F_p &:= \sqrt{F_{py}^2 + F_{px}^2} & F_p &= 5171 \cdot \text{mass} & \text{Total pivot load} \end{aligned}$$

Section A-A Analysis

$$\begin{aligned} H &:= 1.99 \cdot \text{in} \quad t := 0.125 \cdot \text{in} \quad w := 0.50 \cdot \text{in} \quad h := 0.295 \cdot \text{in} & \text{Section A-A parameters} \\ I &:= \frac{t \cdot H^3}{12} + 2 \cdot \left[\frac{(w - t) \cdot h^3}{12} + (w - t) \cdot h \cdot \left(\frac{H}{2} - \frac{h}{2} \right)^2 \right] & I = 0.243 \cdot \text{in}^4 & \text{Inertia at Section A-A} \\ M_a &:= \frac{x_a}{x1} \cdot M_{\text{max}} & M_a &= 8905 \cdot \text{lb} \cdot \text{in} & \text{Moment at Section A-A} \\ \sigma_a &:= \frac{M_a \cdot H}{2 \cdot I} & \sigma_a &= 36520 \cdot \text{psi} & \text{Stress at Section A-A} \\ MS_{23a} &:= \frac{F_{tu}}{\sigma_a} - 1 & MS_{23a} &= 0.04 & \text{Margin of Safety at Section A-A} \end{aligned}$$

Section B-B Analysis

$$\begin{aligned} H &:= 1.744 \cdot \text{in} \quad t := 0.125 \cdot \text{in} \quad w := 0.50 \cdot \text{in} \quad h := 0.25 \cdot \text{in} & \text{Section B-B parameters} \\ I &:= \frac{t \cdot H^3}{12} + 2 \cdot \left[\frac{(w - t) \cdot h^3}{12} + (w - t) \cdot h \cdot \left(\frac{H}{2} - \frac{h}{2} \right)^2 \right] & I = 0.161 \cdot \text{in}^4 & \text{Inertia at Section B-B} \\ M_b &:= \frac{x_b}{x2} \cdot M_{\text{max}} & M_b &= 4452 \cdot \text{lb} \cdot \text{in} & \text{Moment at Section B-B} \\ \sigma_b &:= \frac{M_b \cdot H}{2 \cdot I} & \sigma_b &= 24133 \cdot \text{psi} & \text{Stress at Section B-B} \\ MS_{23b} &:= \frac{F_{cy}}{\sigma_b} - 1 & MS_{23b} &= 0.409 & \text{Margin of Safety at Section B-B} \end{aligned}$$